# **Cavity Quantum Electro-Optic Transduction**

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**Abstract.** The input-output relation between the optical and microwave fields coupled via a cavity electro-optic modulator with red-sideband optical pumping is derived. It is shown that the photon-flux conversion efficiency can in principle reach 100% under a critical coupling condition.

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## INTRODUCTION

Future classical and quantum information processing applications will require coherent conversion of signals between the microwave and optical frequencies. A promising way to achieve the transduction is via the electro-optic effect. Ilchenko *et al.* demonstrated a photonic microwave receiver using a whispering-gallery-mode electro-optic modulator with resonant optical pumping [1], while the author has recently proposed an alternative method of electro-optic transduction using red-sideband optical pumping [2]. The sideband pumping method has the advantage of converting the microwave to an optical wave with a single carrier frequency, rather than one with multiple sidebands as demonstrated in Ref. [1], and can work equally well as a microwave transmitter that converts an optical signal to a microwave. While Ref. [2] focuses on the cooling of thermal microwave fields that can be achieved via red sideband pumping, this paper focuses on the input-output relation between the traveling optical and microwave fields and the resulting conversion efficiency.

#### ANALYSIS



FIGURE 1. Schematic of electro-optic transduction via a cavity electro-optic modulator (EOM).

The setup is illustrated in Fig. 1. Let *a* and *b* be the intra-cavity optical and microwave annihilation operators at frequencies  $\omega_a$  and  $\omega_b$ , respectively. If the optical cavity is pumped at the red-detuned frequency  $\omega_a - \omega_b$  with amplitude  $\alpha_-$  (taken to be real here without loss of generality), we obtain the following equations of motion [2]:

$$\frac{da}{dt} = ig\alpha_{-}b - \frac{\gamma_{a}}{2}a + \sqrt{\gamma_{a}}A, \qquad A' = \sqrt{\gamma_{a}}a - A, \qquad (1)$$

$$\frac{db}{dt} = ig\alpha_{-}a - \frac{\gamma_{b}}{2}b + \sqrt{\gamma_{b}}B, \qquad B' = \sqrt{\gamma_{b}}b - B, \qquad (2)$$

where g is the electro-optic coupling constant defined in Ref. [2],  $\gamma_{a,b}$  are the cavity decay rates, A and B are the input optical and microwave fields and A' and B' are the output fields. Our goal is to express A' and B' in terms of A and B only. Let us first diagonalize the system matrix given by

$$F \equiv \begin{pmatrix} -\gamma_a/2 & ig\alpha_- \\ ig\alpha_- & -\gamma_b/2 \end{pmatrix},\tag{3}$$

which has eigenvalues given by

$$\lambda_{\pm} = -\frac{1}{2} \left( \frac{\gamma_a}{2} + \frac{\gamma_b}{2} \right) \pm ig\alpha_{-}\cos\theta, \qquad \cos\theta \equiv \sqrt{1 - \left[ \frac{1}{2g\alpha_{-}} \left( \frac{\gamma_a}{2} - \frac{\gamma_b}{2} \right) \right]^2}.$$
(4)

The eigenvector matrix is

$$V = \begin{pmatrix} 1 & 1\\ e^{-i\theta} & -e^{i\theta} \end{pmatrix},\tag{5}$$

so we can re-express  $c \equiv (a, b)^T$  in terms of eigenmode operators  $u \equiv (u_+, u_-)^T$  as

$$c \equiv \begin{pmatrix} a \\ b \end{pmatrix} = Vu = \begin{pmatrix} 1 & 1 \\ e^{-i\theta} & -e^{i\theta} \end{pmatrix} \begin{pmatrix} u_+ \\ u_- \end{pmatrix}.$$
 (6)

The transformed equations of motion become

$$\frac{du}{dt} = V^{-1}FVu + V^{-1}\Gamma C, \qquad \Gamma \equiv \left(\begin{array}{cc} \sqrt{\gamma_a} & 0\\ 0 & \sqrt{\gamma_b} \end{array}\right), \qquad C \equiv \left(\begin{array}{cc} A\\ B \end{array}\right), \quad (7)$$

where  $V^{-1}FV$  is diagonal with components  $\lambda_{\pm}$ . Neglecting the initial conditions for *u*, which decay exponentially, *u* in the frequency domain becomes

$$u(\omega) = H(\omega)V^{-1}\Gamma C(\omega), \quad H(\omega) \equiv \begin{pmatrix} 1/(-i\omega - \lambda_{+}) & 0\\ 0 & 1/(-i\omega - \lambda_{-}) \end{pmatrix}.$$
(8)

The output fields can hence be expressed in terms of the input fields by

$$C'(\omega) \equiv \begin{pmatrix} A'(\omega) \\ B'(\omega) \end{pmatrix} = \Gamma c(\omega) - C(\omega) = S(\omega)C(\omega), \quad S(\omega) \equiv \Gamma V H(\omega)V^{-1}\Gamma - I,$$
(9)

*I* being the identity matrix and *S* being the scattering matrix. Explicitly,

$$\begin{pmatrix} A'(\omega) \\ B'(\omega) \end{pmatrix} = \begin{pmatrix} S_{AA}(\omega) & S_{AB}(\omega) \\ S_{BA}(\omega) & S_{BB}(\omega) \end{pmatrix} \begin{pmatrix} A(\omega) \\ B(\omega) \end{pmatrix}.$$
 (10)

For signals with bandwidths much smaller than  $|\lambda_{\pm}|$ , we can consider the scattering matrix *S* at  $\omega = 0$  only:

$$S(0) = \begin{pmatrix} \cos\phi & i\sin\phi \\ i\sin\phi & \cos\phi \end{pmatrix}, \quad \cos\phi \equiv \frac{1 - G_0}{1 + G_0}, \quad \sin\phi \equiv \frac{2\sqrt{G_0}}{1 + G_0}, \quad G_0 \equiv \frac{4g^2\alpha_-^2}{\gamma_a\gamma_b}.$$
(11)

Note that this  $G_0$  is exactly the same as the  $G_0$  defined in Ref. [2] that quantifies the cooling efficiency. The conversion efficiency in terms of the photon flux is thus

$$|S_{AB}|^2 = |S_{BA}|^2 = \frac{4G_0}{(1+G_0)^2},$$
(12)

which is the same for both up-conversion and down-conversion. The efficiency reaches 100% for a finite  $G_0$ :

$$G_0 = 1,$$
  $|S_{AB}|^2 = |S_{BA}|^2 = 1,$  (13)

which can be understood as a *critical coupling* phenomenon. Furthermore, since *S* is unitary, the transduction is in principle a *noiseless* operation.

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### REFERENCES

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